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SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered) READ INSTRUCTIONS BEFORE COMPLETING FORM REPORT DOCUMENTATION PAGE REPORT NUMBER 2. GOVT ACCESSION NO. 3. RECIPIENT'S CATALOG NUMBER SAM-TR-79-20 5. TYPE OF REPORT & PERIOD COVERED TITLE (and Subset MEASURED EFFECTS OF 450-, 350-, and 250-MHz Final rept. PULSED AND 26-MHz CW RADIOFREQUENCY FIELDS ON Jul 1976 - Oct 2978 CARDIAC PACEMAKERS 6. PERFORMING ORG. REPORT NUMBER 8. CONTRACT OR GRANT NUMBER(s) 7. AUTHOR(s) Kenneth A./Hardy/ M.S. 9. PERFORMING ORGANIZATION NAME AND ADDRESS 10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS USAF School of Aerospace Medicine (RZP) 62202F Aerospace Medical Division (AFSC) 7757-01-46 Brooks Air Force Base, Texas 78235. CONTROLLING OFFICE NAME AND ADDRESS 12. REPORT DATE USAF School of Aerospace Medicine (RZP) Jun 2979 Aerospace Medical Division (AFSC) 13. NUMBER OF PAGES Brooks Air Force Base, Texas 78235 14. MONITORING AGENCY NAME & ADDRESS(If different from Controlling Office) 15. SECURITY CLASS. (of this report) Unclassified 15a. DECLASSIFICATION/DOWNGRADING 16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited. 17. DISTRIBUTION STATEMENT (of the ebstract entered in Block 20, If different from Report) 18. SUPPLEMENTARY NOTES 19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Cardiac pacemakers Electromagnetic interference and pacemakers Radiofrequency radiation effects on pacemakers Microwave radiation effects on pacemakers 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Tests were performed to measure the effects of 450-, 350-, and 250-MHz pulsed and 26-MHz CW radiofrequency radiation on cardiac pacemakers. Thirty-three pacemaker models from fourteen different manufacturers were tested both in a free field and simulated implant configuration. The test results presented indicated that the majority of the manufacturers represented had succeeded in producing EMI-resistant pacemakers.

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MEASURED EFFECTS OF 450-, 350-, AND 250-MHz PULSED AND 26-MHz CW RADIOFREQUENCY FIELDS ON CARDIAC PACEMAKERS

INTRODUCTION

Electromagnetic interference (EMI) of medical prosthetic devices such as the cardiac pacemaker is a unique biological effect of nonionizing radiofrequency radiation. The potential hazard of such interactions was well established soon after the development of the demand-type pacemaker, which makes up the majority of currently implanted pacemakers. Demand pacemakers sense the depolarizations of the heart muscle activity and produce their own depolarization signals (electrical stimulus) only if the normal heart depolarizations are not present. Energy pulses induced externally via the pacemaker leads or circuitry can erroneously cause the pacemaker to inhibit its needed output. In addition, in some pacemakers, depending on the electronic circuitry, EMI can induce changes in pacemaker pulse rate of sufficient magnitude to be considered hazardous without actually inhibiting pacemaker output.

Since 1972 the USAF School of Aerospace Medicine (USAFSAM) has been conducting tests on the EMI characteristics of cardiac pacemakers, both in the USAFSAM radiofrequency radiation (RFR) laboratory and in close proximity to a variety of Air Force RF emitters (1-5). During this period of time, the manufacturers have continuously improved the EMI characteristics of their product and have significantly reduced the potential hazard. The following report provides the results of tests conducted at USAFSAM in 1976-1978 on some of the more recently available pacemakers and serves as an addendum to the previous reports.

TEST PROCEDURES

Implant Simulation

Realistic assessment of the effects of radiofrequency electromagnetic radiation (EMR) on cardiac pacemakers requires retual implant conditions or accurate simulation of implantation. At USAFSAM a pacemaker test chamber is used to simulate implant conditions. The chamber is designed to specifications set forth in a protocol for cardiac pacemaker testing drafted by the Association for the Advancement of Medical Instrumentation (AAMI). The chamber consists of an 80 x 40 x 20 cm container made of 5-cm-thick low dielectric plastic foam (density of 0.035 g/cm²). This container is filled with 0.03 molar saline solution. The pacemaker is placed in the solution on a plastic frame such that

approximately 1 cm of solution lies between the pacemaker and its leads and the anterior (source) side of the container. The pacemaker lead is stretched out horizontally, and the pacemaker response is picked up via 2 x 2 cm copper mesh electrodes placed in the solution at both ends of the container. The signal is fed out via lossy line leads to an electrocardiogram amplifier. The amplified signal in turn is relayed to a strip-chart recorder and Hewlett-Packard Model 5360A computing counter. The computing counter is used to give a direct readout of pacemaker pulse rate. A more complete description of this system can be found in a previous report (4).

Tests were also conducted under "free field" conditions as per the AAMI recommendation. In this mode the pacemakers were exposed in the pacemaker container without the saline solution. An LED fiber optics monitoring system was used to feed the pacemaker output to the computing counter and strip-chart recorder. A complete description of this system can be found elsewhere (6). Only the simulated implant data is presented herein.

Both sides of the pacemaker were tested in accordance with the AAMI protocol; that is, first one, and then the other, side of the pacemaker was exposed to the RF source. In some instances a difference was observed in EMI sensitivity from one side to the other. In this situation the lowest EMI threshold value is presented in this report.

Instrumentation

Four radiation frequencies were used: 26, 250, 350, and 450 MHz. The 26-MHz exposures were conducted under continuous wave (CW) conditions in a copper-screen TEM exposure chamber. The radiation source was provided by a Federal Telephone & Radio Corp. AN/FRT-6B transmitter. The maximum E-field obtained was 850 V/m.

The 250-, 350-, and 450-MHz tests were performed in the USAFSAM RFR anechoic chamber. The radiation source was a Microwave Cavity Laboratory (MCL) Model 15022 power generator, amplified by an MCL Model 10110 power amplifier (up to 1000 W) and fed via an air dielectric "Heliax" transmission line to an EMCO Model 3101 conical longspiral antenna. The maximum E-fields obtained were 270, 300, and 330 V/m, respectively.

The RF fields at the test location were measured with a National Bureau of Standards (NBS) 5-cm dipole antenna field intensity probe. The voltage output of the dipole probe is fed via lossy line to a Kiethly Model 600B electrometer. The E-field was measured as a function of transmitter power output at each test frequency. In the 26-MHz exposures the power output was monitored with a Bird Thruline Model 3122 wattmeter. A Bird Thruline Model 43 wattmeter was used to monitor the power output at 250, 350, and 450 MHz.

The RF field as a function of output power was measured in the empty pacemaker chamber at the pacemaker position. In addition, the field was

mapped across the length of the pacemaker chamber with the power output constant. The E-field distribution across the chamber was found to be approximately "Gaussian." The E-field value listed with the data is the average value across the length of the chamber. The maximum E-field at the center of the chamber was approximately 10% higher than the average value.

Free-field tests were then conducted in the test chamber. The pace-maker performance was monitored as a function of gradually increasing RF output power. Those power levels at which the pacemaker performance was affected were noted on the strip chart recorded along with the measured pacemaker pulse rate as given by the computing counter. When the free-field tests were completed, the chamber was filled with saline solution, and the tests were repeated in the simulated-implant mode. The pacemakers were tested on both sides in both modes.

TEST RESULTS

A total of 33 pacemaker models from 14 different manufacturers were evaluated to establish their relative electromagnetic interference susceptibilities as a function of the radiation frequency, pulse width, and Efield intensity.

Twenty were current production models or test models planned for production at the time of the initiation of the study provided by the manufacturers for evaluation. The remainder were different models, chosen from the USAFSAM pacemaker inventory, that had been tested previously for EMI susceptibility at 450 MHz under simulated-implant conditions (3, 4). Their inclusion served (1) to check the validity of current EMI test procedures, and (2) to confirm prior EMI test results under more accurately controlled laboratory conditions.

The test results are summarized in Table 1. A survey of the manufacturers at the time of the writing of this report indicates that eighteen of the models tested were no longer in production. Of these obsolete models, thirteen (72%) exhibited definite EMI susceptibility below 200 V/m, the required E-field limit recommended in the AAMI protocol. Of the fifteen models still in current production or planned for production, ten (67%) exhibited no EMI susceptibility below 200 V/m, thereby showing a marked improvement in the EMI reliability of current pacemaker models.

Of the thirteen models with previous EMI test data, agreement with prior test results was achieved with regard to susceptibility or non-susceptibility for eleven cases. The two exceptions were the CPI Models 301UD and 401BD, which exhibited EMI susceptibility in the present study, but did not do so previously (4). The former was found to be quite a bit more sensitive on the back (nonlabel) side, which was not looked at in the previous study at 450 MHz. In the case of the 401BD, both sides were equally susceptible at 450 MHz to EMI in the present study.

Two of the manufacturers, American Optical and General Electric, were found to be no longer manufacturing pacemakers. Of the twelve still producing pacemakers, nine had models with EMI thresholds greater than 200 V/m, thus demonstrating that the majority of manufacturers represented had succeeded in developing high-quality EMI-resistant pacemakers.

DISCUSSION

The data in Table 1 illustrates the extent to which pacemaker EMI depends on the emission characteristics of the radiation source. For example, none of the pacemaker models tested exhibited any EMI below 200 V/m for the continuous-wave fields at 26 MHz, whereas 18 pacemaker models exhibited EMI below 200 V/m in the pulsed radiation modes. Of the 15 pacemaker models which exhibited no EMI below 200 V/m in the pulsed radiation modes, the majority were the newer production models or the test models, indicating that most of the manufacturers have succeeded in developing pacemakers that are compatible with the electromagnetic environment.

In general, those pacemakers found to be affected in the "free field" mode of exposure were also found to be affected in the simulated-implant mode, with the EMI thresholds somewhat higher in the latter case, illustrating the effect of shielding as a protective factor. In addition, testing of the pacemakers on both sides in some cases revealed differences in EMI threshold, thus illustrating the added effect of pacemaker orientation.

CONCLUSION

Cardiac pacemaker EMI is strongly dependent on frequency, pulse width, E-field level, and pulse repetition rate of the incident radiation signal. Also important are shielding and pacemaker orientation. These test results (Table 1) provide substantial evidence of continued overall improvement in the EMI characteristics of currently marketed cardiac pacemakers. These findings demonstrate the technical feasibility of manufacturing high-quality EMI-resistant pacemakers, thus resolving a problem that existed with devices marketed in the early 1970s.

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TABLE 1. CARDIAC PACEMAKER EMI THRESHOLDS IN VOLTS/METER
AS A FUNCTION OF FREQUENCY AND PULSE WIDTH
(SIMULATED-IMPLANT, PULSE REPETITION RATE, 10 PPS)

		450 MHz Pulse width	ŧ		350 MHz Pulse width	. £	•	250 MHz Pulse width	£	26 MHz
Pacemaker	20 ms	1 ms	10 µs	20 ms	J ms	10 µs	20 ms	1 ms	10 иѕ	CM
American 1613	>360	>360	>360	N.T.	Ä.T.	N.T.	r.T.	N.T.	N.T.	N.T.
American Optical 281003 N.L.I.P. 281143a N.L.I.P.	25 265(5)	25 >330	45 >330	>330	>300	72 >300	20 >270	20 >270	32 >270	670 >850
Biotronik IDP-44 IDP-54	110(5)	125(5)	>330	60(5)	60(5) 70(5)	×300 ×300	20 45(5)	20	145 >270	>850 390
Cardiac Pacemakers, 301UD N.L.I.P. 401BD N.L.I.P. 501UD	Inc. 85(5) 30(5) >330	145(5) 75(5) >330	×330 ×330	55 110 >300	120 185 >300	×300 ×300	30(5) 20(5) >270	50 30(5) >270	>270 >270 >270 >270	550 620 230
Coratomic L-500	>360	>360	>360	N.T.	F. Y	N.T.	N.T.	 ⊢.	N.T.	N.T.
Cordis Stanicor K "DX"b Stanicor K "D"b Omni Stanicor 162C N.L.I.P.	>330 >330 20	>330 >330 20	>330 >330 80(5)	>300 >300 20(5)	>300 >300 20	×300 ×300 230	>270 >270 20	>270 >270 20	>270 >270 30	×850 ×850 ×850
General Electric A2075Ab N.L.I.P.	165(5)	260	235	90(5)	30(5)	105	20	20	>270	099
Medcor "C" (Equiv 3-70C) 3-70A N.L.I.P. 3-70B N.L.I.P.	>330 20(5) 20(5)	>330 25(5) 30(5)	>330 70(5) 90(5)	>300 20(5) 20(5)	>300 20(5) 25	>300 110 35(5)	>270 20(5) 20(5)	>270 20(5) 20	>270 75(5) 230(5)	720 >850 >850

a3 pacers tested bTest model

TABLE 1 (continued)

Pacemaker Medtronic 5842 N.			450 MHz Pulse width 1 ms 25	10 us	20 ms	350 MHz Pulse width			250 MHz Pulse width 1 ms		26 MHz CW CW
5942 5944 5972 5973 9000	N. L. I. P	×330 ×330 ×330 ×330 ×330 ×330 ×330 ×330	30(5) 85 8330 8330 8330 25	7333 7333 130 130 130 130	× 300 × 300 × 300 × 20	7.1 140 7300 7300 7300 25	× × × × × × × × × × × × × × × × × × ×	20 185(5) >270 >270 >270 >270 >270	×270 ×270 ×270 ×270 ×270 ×270	230 270 270 270 270 270 270	×850 ×850 ×850 ×850 ×850
Pacesetter BD-101	Pacesetter Systems Inc. BD-101 N.L.I.P.	. >330	>330	>330	>300	>300	>300	>270	>270	>270	760
Starr-Edwa 8114 8116	Starr-Edwards 8114 N.L.I.P. 8116 N.L.I.P.	30(5)	30(5)	×330	>300	×300	>300	20 >270	20 >270	35 >270	620 >850
Edwards La 81165 205 215	Edwards Laboratories 8116S N.L.I.P. 20S 21S	×330 ×330	×330 ×330	×330 ×330 ×330	×300 ×300 ×300	×300 ×300	×300 ×300	>270 >270 >270	×270 ×270 ×270	>270 >270 >270	×850 ×850 ×850
Stimtech 3821	N.L.I.P.	30	105	>330	50	45	>300	35	110(5)	>270	260
Vitatron Medi MIP-40RT N MIP-42RT1.0 MIP-42RT0.5	Vitatron Medical MIP-40RT N.L.I.P. MIP-42RT1.0 MIP-42RT0.5	25(5) 25 30(5)	35(5) 90(5)	310 110 200(5)	20(5) 20 20	20 50(5) 55(5)	300	20(5) 20 20	2000	40 270 105(5)	850 350 590

270, and 850 V/m for the 450-, 350-, 250-, and 26-MHz 300 The maximum E-fields available were 360, frequencies, respectively. NOTE:

(5) These EMI thresholds were observed at 5 pps.

N.T. Not tested.

N.L.I.P. No longer in production.